Name _____

Instructor

Section/College

Electrical Engineering Advancement Exam III

FALL SEMESTER 2020

<u>CLOSED BOOK, CLOSED NOTES</u> <u>2 HOUR TIME LIMIT</u>

CALCULATORS ARE ALLOWED

(calculators without communication capability only) ELECTRONIC DEVICES WITH COMMUNICATION CAPABILITY (electronic devices such as cell phone, pagers, and iPads) MAY NOT BE USED DURING THE EXAMINATION

(If such devices ring or are visible, a 10% penalty will be given for the first occurrence and exam failure for the second.)

There are 10 problems: please look over the exam to make sure that you have 10 different problems. **Do any eight (8) problems!** Draw a large X through the two problems that you do not want to be graded. If you do not indicate which problems you want to leave out, the first 8 problems will be graded.

Do all work for each problem only on the page supplied for that problem (you may use both sides). **DO NOT**, for instance, continue Problem #3 on the back of Problem #2. Extra blank paper will be supplied if needed. If extra paper is used, show the additional work for each problem on a separate sheet and staple the extra sheet(s) to the appropriate problems.

(1)

(c)

(a) [5 points] For intrinsic semiconductors at equilibrium, the electron concentration (number of electrons per unit volume) at room temperature is ??? Circle the one correct choice.

Equal to 1.0 x 10²² cm⁻³ Equal to the hole concentration Equal to 4 electron per atom times the number of atoms per cm³ None of the above are true

(b) [5 points] Because the energy-gap E_G of crystalline silicon is bigger than that of crystalline germanium, the electron concentration of intrinsic silicon has what relationship to the electron concentration of intrinsic germanium at room temperature? Circle the one correct choice.

$\mathbf{n}_{\mathrm{o},\mathrm{Si}} > \mathbf{n}_{\mathrm{o},\mathrm{Ge}}$	$\mathbf{n}_{\mathrm{o},\mathrm{Si}} < \mathbf{n}_{\mathrm{o},\mathrm{Ge}}$	Undetermined for given information	
[5 points] In a pn step which direction (i.e. is po	junction diode, the e	lectric field inside the detection of th	epletion region points in

From the n region to the p region From the p region to the n region Direction depends on bias voltage

(d) [10 points] Sketch the energy band diagram for a step pn junction for forward bias conditions. Label the edge of the conduction band and the valence band, the Fermi level in both n and p regions, the difference qV_A .

An abrupt silicon p-n junction has an acceptor concentration 10^{16} cm⁻³ (no donors) in the p-side and a donor concentration 10^{16} cm⁻³ (no acceptors) in the n-side, respectively. The intrinsic carrier concentration of silicon is 1.50 x 10^{10} cm⁻³ at room temperature (300 K). Answer the following questions assuming all dopants are ionized at room temperature.

(a) [7 points] Calculate the potential difference across the junction at equilibrium (i.e. contact potential V_o).

 $V_{\theta} =$

(2)

(b) [6 points] Calculate the ratio of p-side depletion width x_{po} versus n-side depletion width x_{no} at equilibrium, i.e. x_{po}/x_{no} .

 $x_{po}/x_{no} =$

(c) [6 points] Calculate the total potential difference in eV across the junction when a forward bias voltage of $V_A = +0.30$ V is applied, i.e. determine the difference between the band edge energy on the p-side of the junction with respect to the n-side.

(d) [6 points] Calculate the ratio of total depletion width at equilibrium versus total depletion width with a forward bias of $V_A = +0.20$ V, i.e. W_o/W .

 $W_o/W =$

(3) Consider an idealized diode with a reverse saturation current 0.01 mA and an abrupt turn-on voltage of 0.70 V (assume no breakdown and operation away from the knee of the diode curve). For the circuit shown, both resistors are 100 Ω , the constant source is V_P = 5.0 V, and the time-dependent source is V_s = 20 sin(ω t) V.



(a) [12 Points] State the bias condition of the diode. Calculate the peak positive voltage V and the associated current I_d through the diode. Calculate the answers to at least four decimal points (x.xxxx).

V = $I_d =$

(b) [13 Points] State the bias condition of the diode. Calculate the peak negative voltage V and the associated current I_d through the diode.

(4)

Consider the npn-transistor Darlington amplifier circuit shown with three npn BJTs. The transistors are identical with a nominal beta $\beta = \beta_1 = \beta_2 = \beta_3 = 10$, a turn-on voltage $V_{to} = 0.70$ V, and a saturation emittercollector voltage $V_{EC(SAT)} = 0.20$ V. The circuit values are $V_{CC} = 100$ V, $V_{BB} = 7.1$ V, $R_{BI} = 10.0$ k Ω , and $R_C = 10 \Omega$.



(a) [18 points] Calculate the currents i_{C1} , i_{C2} , and i_{C3} .

i_{C1} =

 $i_{C3} =$

(b) [7 points] Calculate the total current through the resistor \mathbf{R}_{C} and the voltage across \mathbf{R}_{C} , i.e. i_{CTotal} and V_{o} .

 $i_{C2} =$

i_{CTotal} =

 $V_o =$





(a) [12 points] Calculate the transistor currents i_B and i_E .

 $i_B =$ $i_E =$

(b) [13 points] Calculate the operating point i_C and v_{EC} .

*i*_C = _____

 $v_{EC} =$

(a) [5 points] For the inverter MOSFET circuit shown, the enhancement-mode p-channel MOSFET has parameters V_{on} and K and the depletion-mode p-channel MOSFET has parameters V_{po} and I_{SDS}. For the upper or load MOSFET, sketch the IV characteristic i_{SD2} vs. v_{SD2} . State the control voltage v_{SG2} value and label the axes and any key voltage or current values.



- (b) [5 points] For the inverter MOSFET circuit shown in part a, the enhancement-mode p-channel MOSFET has parameters V_{on} and K and the depletion-mode p-channel MOSFET has parameters V_{po} and I_{SDS}. Sketch the **load line** for the lower or driver transistor i_{SD1} vs. v_{SD1} . Label the axes and important intercept values.
- (c) [9 points] Consider an n-channel MOSFET circuit with $V_{on} = 3.00$ V, K = 1.00 mA/V², $R_d = 1.00$ k Ω , $V_{DD} = 20.0$ V, and $V_i = 5.0$ V. Calculate the operating point or Q-point, i.e. i_{DS} and v_{DS} .



 $v_{DS} =$

 $i_{DS} =$

(d) [6 points] For the MOSFET circuit in part b with $V_{on} = 3.00$ V, K = 1.00 mA/V², $V_{DD} = 20.0$ V, and $V_i = 5.0$ V, calculate the range of R_d for which the transistor operation stays in saturation.

Range of *R*_d:

Problem Score /25

(6)

- (7)
- (a) [5 points] Consider a p-channel JFET with specifications V_{po} and I_{SDS} . Sketch the saturation curve i_{SD} vs. v_{SG} i.e. the curve for saturation conditions. Label all intercepts.

(b) [20 points] Consider the p-channel JFET circuit shown. The transistor parameters/specifications are $V_{po} = 4.00$ V and $I_{SDS} = 10.0$ mA. The circuit values are $\mathbf{R}_d = 1.70$ k Ω and $V_{DD} = 20.0$ V. Calculate the input voltage v_{SG} ; the operating point or Q-point, i.e. i_{SD} and v_{SD} ; and the load-line intercepts for current and voltage. Sketch the current-voltage characteristic and the load-line on the same graph. Label the operating point (Q-point) and the load-line intercepts.



 $v_{SG} =$

 $v_{SD} =$

 $i_{SD} =$

Voltage-axis intercept = (<u>, 0 A</u>)

Current-axis intercept = (0 V,)

Problem Score /25

- (8)
- (a) [8 points] The OpAmp shown has ideal resistances R_{in} and R_{out} and has a finite open-loop gain A = 20,000. For the circuit shown, calculate V_0/V_s . Express the answer to at least 5 decimal points (x.xxxx).



 $V_0/V_s =$

(b) [7 points] For the OpAmp circuit shown, sketch the equivalent circuit in which the OpAmp is replaced with appropriate circuit elements. Assume **non-ideal** OpAmp parameters.



(c) [3 points] What type of OpAmp circuit is shown in part b? (Circle the best choice.)

Inverting (*V*₀ / *V*_{TH} neg.)

Non-Inverting (*Vo / V*_{TH} pos.)

(d) [7 points] Use the OpAmp circuit shown in part b and assume **ideal** parameters. Consider the OpAmp circuit shown. The OpAmp is ideal. The Thevenin circuit values are $V_{TH} = 5.00 \text{ V}$ and $R_{TH} = 1.00 \text{ k}\Omega$.

The feedback resistor $R_2 = 20.00 \text{ k}\Omega$. Calculate the value of resistor R_1 such that the magnitude of the output voltage to the Thevenin voltage is $|V_O/V_{TH}| = 5$.

 $\mathbf{R}_1 =$

- (9)
- (a) [8 points] Identify the two OpAmp circuits shown. (Select the best answers.)



Circuit ______ is a Differentiating circuit ($V_o = - \text{RC } d(V_s)/dt$) Circuit ______ is a Integrating ($V_o = (-1/\text{RC}) \int (V_s) d\tau$

(b) [8 points] Consider the OpAmp circuit shown. Assume an ideal OpAmp. The resistance values + $R_1 = 1.00 \text{ k}\Omega$, $R_2 = 5.00 \text{ k}\Omega$,

 $R_3 = 2.00 \text{ k}\Omega$, and $R_4 = 2.00 \text{ k}\Omega$.

Operation is in the linear range.

Calculate the output V_0 as a function of v_1 when $v_2 = 0$. Hint: Use superposition.



$$V_{O}|_{v^{2}=0} = V_{OI} = ($$
______) v_{I}

(c) [9 points] Consider the same OpAmp circuit. Assume an **ideal** OpAmp. The resistance values are the same as in (b) and are

 $\boldsymbol{R}_1 = 1.00 \text{ k}\Omega, \, \boldsymbol{R}_2 = 5.00 \text{ k}\Omega,$

 $R_3 = 2.00 \text{ k}\Omega$, and $R_4 = 2.00 \text{ k}\Omega$.

Operation is in the linear range.

Calculate the output V_0 as a function of v_2 when $v_1 = 0$. Hint: Use superposition.



$$V_{O}|_{v1=0} = V_{O2} = ($$
______) v_{2}



(10)

Consider the Si pin photodiode circuit shown with source voltage V_s and resistance $\mathbf{R} = 6000$ Ohms. The bandgap energy for Si is $E_G = 1.12$ eV. The reverse saturation current (for "dark" conditions) is 0.10 mA. Light of wavelength $\lambda = 0.900$ µm is incident; the efficiency is 0.90. Assume the photodiode voltage |V| >> kT/q and room temperature.



 (a) [5 points] For photoconductive operation as described in the lecture notes, what is the correct bias condition for the photodiode? Choose (circle) the correct choice.

Forward bias No Bias Reverse Bias

(b) [5 points] Calculate the photon energy E_P for this wavelength. Express the photon energy in eV.

 $\mathbf{E}_{\mathbf{P}} =$

(c) [10 points] For an absorbed optical power P at this wavelength $\lambda = 0.900 \,\mu\text{m}$, the photo-induced current is $I_{\text{light}} = 1.0 \,\text{mA}$. Calculate the absorbed optical power in W.

P=

(d) [5 points] For the photo-induced current of $I_{light} = 1.0$ mA, the operating voltage is V = -7.50 V. Calculate the needed source voltage V_s .

*V*_S =



EE 2200 Equation Sheet



$$\begin{split} \rho(T) &= \rho_{20} [1 + \alpha_{20} (T - 20)] & (E_F - E_i) = kT \ln \left(\frac{n_0}{n_i}\right) \\ n_0 + N_a^- &= p_0 + N_d^+ & (E_F - E_i) = -kT \ln \left(\frac{p_0}{n_i}\right) \\ n_0 p_0 &= n_i^2 & n_0 = n_i e^{\frac{(E_F - E_i)}{kT}} \end{split}$$

$$\begin{split} J &= q D_{n} \frac{dn}{dx} - q D_{p} \frac{dp}{dx} & p_{0} = n_{i} e^{\frac{-(E_{F} - E_{i})}{kT}} \\ J &= q (n_{o} \mu_{n} + p_{0} \mu_{p}) E = \sigma E & V_{0} = \frac{kT}{q} ln \left[\frac{\left(N_{ap}^{-} - N_{dp}^{+} \right) \left(N_{dn}^{+} - N_{an}^{-} \right)}{n_{i}^{2}} \right] \\ \frac{D_{n}}{\mu_{n}} &= \frac{kT}{q} & q V_{0} = (E_{F} - E_{in}) - (E_{F} - E_{ip}) \\ \frac{D_{p}}{\mu_{p}} &= \frac{kT}{q} & \left(N_{ap}^{-} \right)_{Eff} x_{p0} = (N_{dn}^{+})_{Eff} x_{n0} \\ W_{0} &= \left\{ \frac{2\epsilon_{0}\epsilon_{r}V_{0}}{q} \left[\frac{\left(N_{ap}^{-} \right)_{Eff} + \left(N_{dn}^{+} \right)_{Eff}}{\left(N_{ap}^{-} \right)_{Eff} + \left(N_{dn}^{+} \right)_{Eff}} \right] \right\}^{1/2} & I = I_{0} \left[e^{\left(\frac{qV}{kT} \right)} - 1 \right] \\ W &= \left\{ \frac{2\epsilon_{0}\epsilon_{r}(V_{0} - V_{A})}{q} \left[\frac{\left(N_{ap}^{-} \right)_{Eff} + \left(N_{dn}^{+} \right)_{Eff}}{\left(N_{ap}^{-} \right)_{Eff} \left(N_{dn}^{+} \right)_{Eff}} \right] \right\}^{1/2} \end{split}$$

$\begin{array}{l} \underline{\text{BJT Relationships}}\\ i_{B} = \frac{1}{\beta} i_{C} & i_{E} = i_{B} + i_{C} & \alpha_{0} = \frac{\beta}{\beta+1} \\ \\ \alpha_{F} = \frac{i_{Cn}}{i_{En}} & \text{or} & \alpha_{F} = \frac{i_{Cp}}{i_{Ep}} & \gamma = \frac{i_{En}}{i_{En}+i_{Ep}} & \text{or} & \gamma = \frac{i_{Ep}}{i_{En}+i_{Ep}} \end{array}$

Saturation Conditions

$$\begin{split} v_{DG} &= v_{DS} - v_{GS} \geq V_{po} & v_{GD} = v_{SD} - v_{SG} \geq V_{po} \\ v_{DS} - v_{GS} \geq -V_{on} & v_{SD} - v_{SG} \geq -V_{on} \end{split}$$

FET Relationships

$$\begin{split} i_{DS} &= I_{DSS} \left[2 \left(1 + \frac{v_{GS}}{v_{po}} \right) \left(\frac{v_{DS}}{v_{po}} \right) - \left(\frac{v_{DS}}{v_{po}} \right)^2 \right] \\ i_{DS} &= I_{DSS} \left[2 \left(1 + \frac{v_{SG}}{v_{po}} \right) \left(\frac{v_{SD}}{v_{po}} \right) - \left(\frac{v_{SD}}{v_{po}} \right)^2 \right] \\ i_{SD} &= I_{SDS} \left[2 \left(1 + \frac{v_{SG}}{v_{po}} \right) \left(\frac{v_{SD}}{v_{po}} \right) - \left(\frac{v_{SD}}{v_{po}} \right)^2 \right] \\ i_{DS} &= KV_{on}^2 \left[2 \left(\frac{v_{GS}}{v_{on}} - 1 \right) \left(\frac{v_{DS}}{v_{on}} \right) - \left(\frac{v_{DS}}{v_{on}} \right)^2 \right] \\ i_{SD} &= KV_{on}^2 \left[2 \left(\frac{v_{SG}}{v_{on}} - 1 \right) \left(\frac{v_{SD}}{v_{on}} \right) - \left(\frac{v_{SD}}{v_{on}} \right)^2 \right] \\ i_{SD} &= KV_{on}^2 \left[2 \left(\frac{v_{SG}}{v_{on}} - 1 \right) \left(\frac{v_{SD}}{v_{on}} \right) - \left(\frac{v_{SD}}{v_{on}} \right)^2 \right] \\ i_{SD} &= KV_{on}^2 \left[2 \left(\frac{v_{SG}}{v_{on}} - 1 \right) \left(\frac{v_{SD}}{v_{on}} \right) - \left(\frac{v_{SD}}{v_{on}} \right)^2 \right] \\ i_{SD} &= KV_{on}^2 \left[2 \left(\frac{v_{SG}}{v_{on}} - 1 \right) \left(\frac{v_{SD}}{v_{on}} \right) - \left(\frac{v_{SD}}{v_{on}} \right)^2 \right] \\ i_{SD} &= KV_{on}^2 \left[2 \left(\frac{v_{SG}}{v_{on}} - 1 \right) \left(\frac{v_{SD}}{v_{on}} \right) - \left(\frac{v_{SD}}{v_{on}} \right)^2 \right] \\ i_{SD} &= KV_{on}^2 \left[2 \left(\frac{v_{SG}}{v_{on}} - 1 \right) \left(\frac{v_{SD}}{v_{on}} \right) - \left(\frac{v_{SD}}{v_{on}} \right)^2 \right] \\ i_{SD} &= KV_{on}^2 \left[2 \left(\frac{v_{SG}}{v_{on}} - 1 \right) \left(\frac{v_{SD}}{v_{on}} \right) - \left(\frac{v_{SD}}{v_{on}} \right)^2 \right] \\ i_{SD} &= KV_{on}^2 \left[2 \left(\frac{v_{SG}}{v_{on}} - 1 \right) \left(\frac{v_{SD}}{v_{on}} \right) - \left(\frac{v_{SD}}{v_{on}} \right)^2 \right] \\ i_{SD} &= KV_{on}^2 \left[2 \left(\frac{v_{SG}}{v_{on}} - 1 \right) \left(\frac{v_{SD}}{v_{on}} \right) - \left(\frac{v_{SD}}{v_{on}} \right)^2 \right] \\ i_{SD} &= KV_{on}^2 \left[2 \left(\frac{v_{SG}}{v_{on}} - 1 \right) \left(\frac{v_{SD}}{v_{on}} \right) - \left(\frac{v_{SD}}{v_{on}} \right)^2 \right] \\ i_{SD} &= KV_{on}^2 \left[\frac{v_{SD}}{v_{on}} - 1 \right] \left(\frac{v_{SD}}{v_{on}} \right) - \left(\frac{v_{SD}}{v_{on}} \right)^2 \right] \\ i_{SD} &= KV_{on}^2 \left[\frac{v_{SD}}{v_{on}} - 1 \right] \left(\frac{v_{SD}}{v_{on}} \right) - \left(\frac{v_{SD}}{v_{on}} \right)^2 \right] \\ i_{SD} &= KV_{on}^2 \left[\frac{v_{SD}}{v_{on}} \right]$$

$$\begin{split} f &= \frac{c}{\lambda} & E_{p} = hf = \frac{hc}{\lambda} \\ I &= I_{0}e^{-\alpha_{L}x} & v_{p} = \frac{c}{n} \\ I &= I_{0}\left[e^{\frac{qV_{d}}{kT}} - 1\right] - I_{light} & I_{light} = \frac{\eta qP\lambda}{hc} \end{split}$$